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WHS-026-1

Copy \_\_\_ of \_\_\_

Pages 19

9 June 1966

- SIMULATION STUDIES
- BACKUP ANALOG ACQUISITION  
AND TRACKING UNIT

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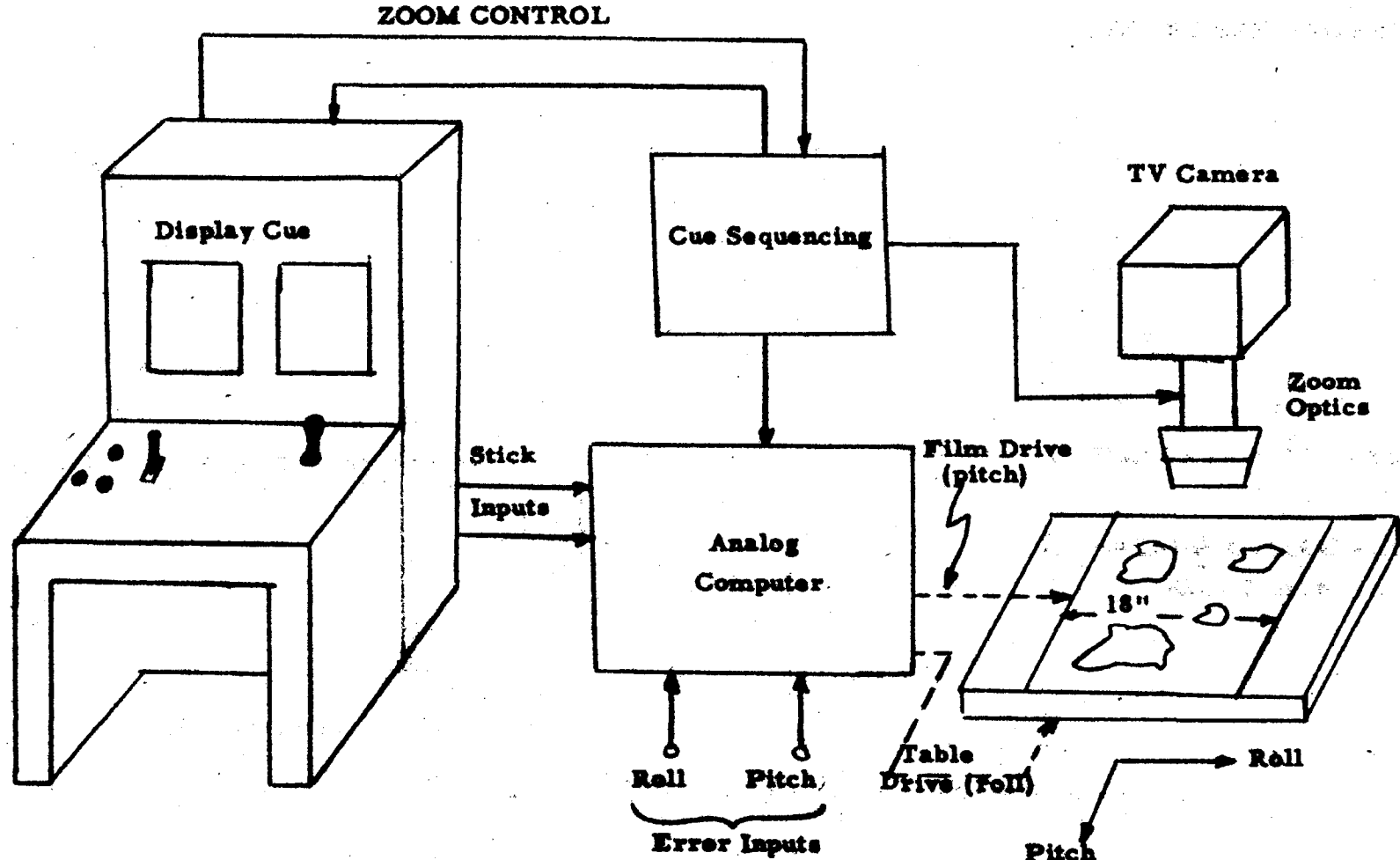
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**SIMULATION STUDIES**

- **PERFORMED ON LMSC SIMULATOR 6/1-2/66**
  
- **OPERATORS (FLIGHT CREW)**
  - **R. TRULY**
  - **J. TAYLOR**
  
- **PURPOSE**
  - **EXTEND DATA ON MANUAL TRACKING CAPABILITY TO  
> 1% RATE AIDING ERRORS**
  - **EVALUATE UTILITY OF AN AUGMENTED CONTROL STICK**
  
- **OBJECTIVES**
  - **PROVIDE BASIS FOR EVALUATION OF EFFECTIVENESS  
OF LESS ACCURATE RATE AIDING TECHNIQUES  
(E. G., A SIMPLE ANALOG BACKUP TO THE  
DIGITAL COMPUTER)**
  - **PROVIDE BASIS FOR FURTHER STUDY OF CONTROL  
SYSTEM DESIGN WRT MAN**

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**DISPLAY POWER:**

ACQ: 8.4 - 25.2

MADE: 100 - 165

**TABLE DRIVE CAPABILITY (EQUIV.)**

ACQ: 7.5°/sec max., .075°/sec min

MADE: 4.1° sec max  
5-T/hr. rotation

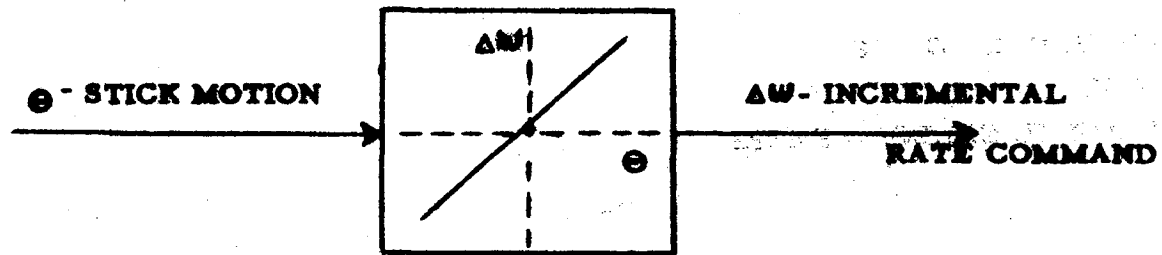
**LMBC SIMULATOR**

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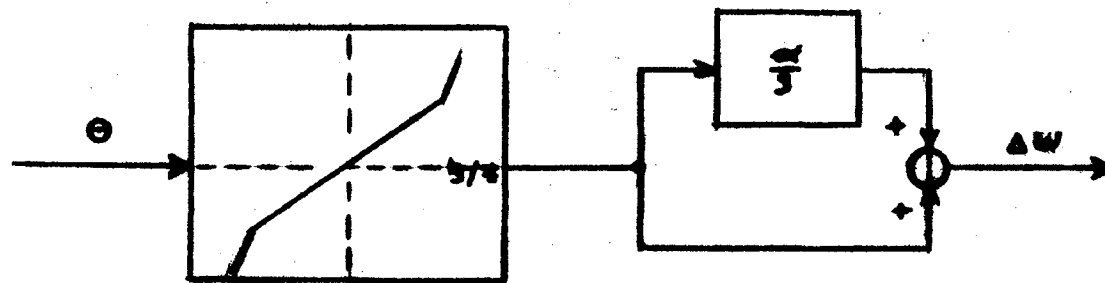
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CONTROL STICK TRANSFER FUNCTIONS

• "BASELINE"



• NONLINEAR ACCELERATION AUGMENTED STICK



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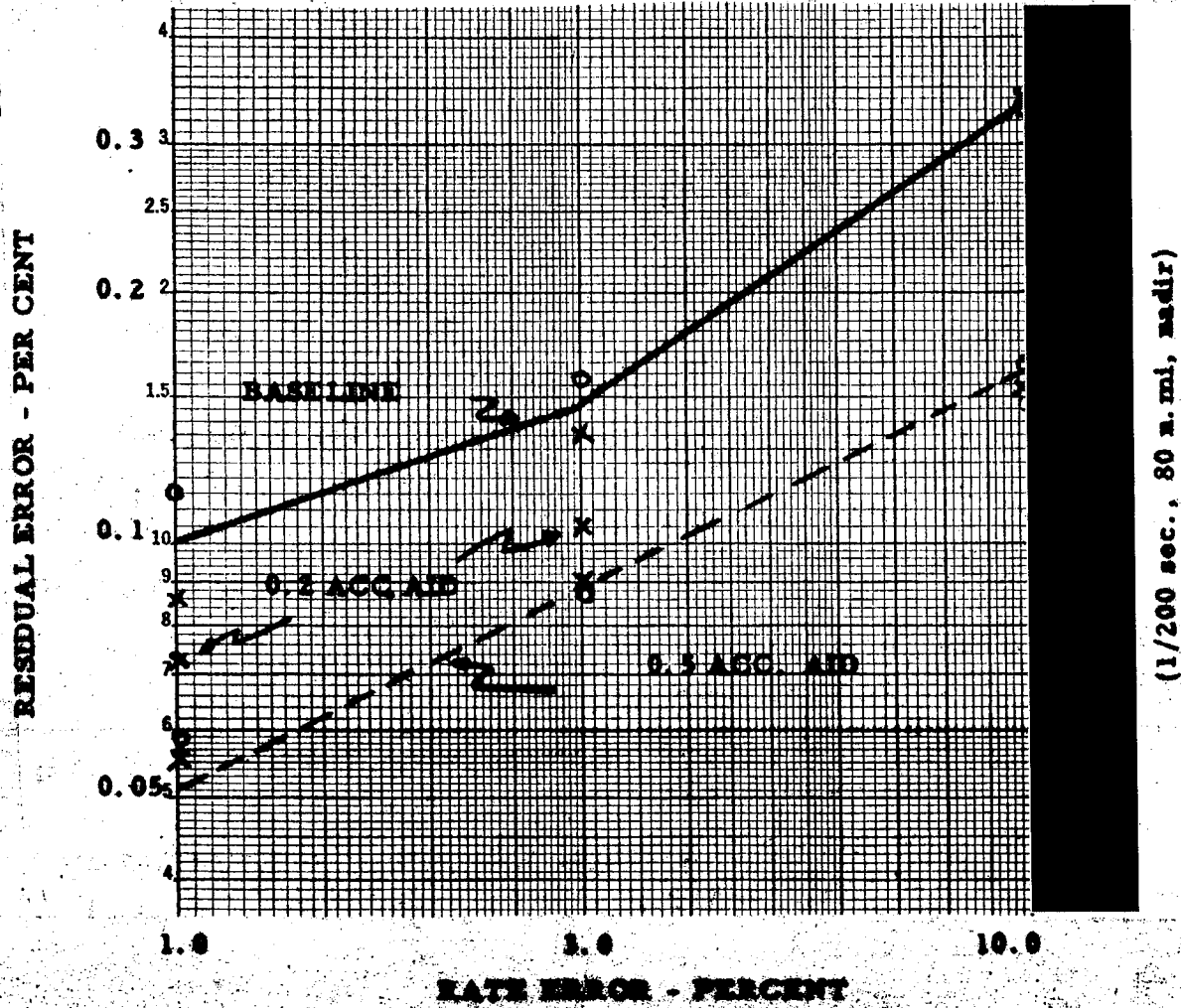
STUDY CASES

<u>PERCENT ERROR</u>	<u>STICK TYPE</u>	<u>STICK GAIN</u>	<u>ACCEL. AUGMENTATION</u>
1	LINEAR	1	0
3	"	3	0
10	"	10	0
1	NONLINEAR	1	0
3	"	3	0
1	"	1	.2
3	"	1	.2
10	"	1	.2
3	"	1	.5
10	"	1	.5
10	"	2	.5

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RATE  
ERROR

ACCELERATION  
AUGMENTATION

BASELINE  
TYPICAL

10 X



0

BEFORE  
LEARNING  
(3RD TRIAL)

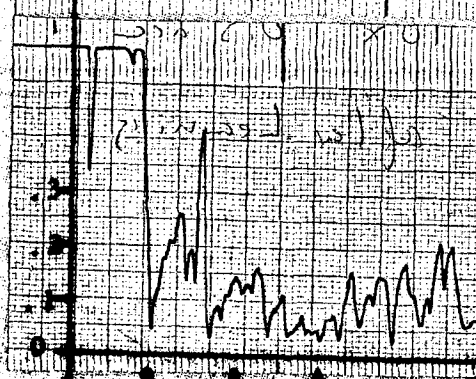
3 X



0.5

AFTER  
LEARNING

10 X

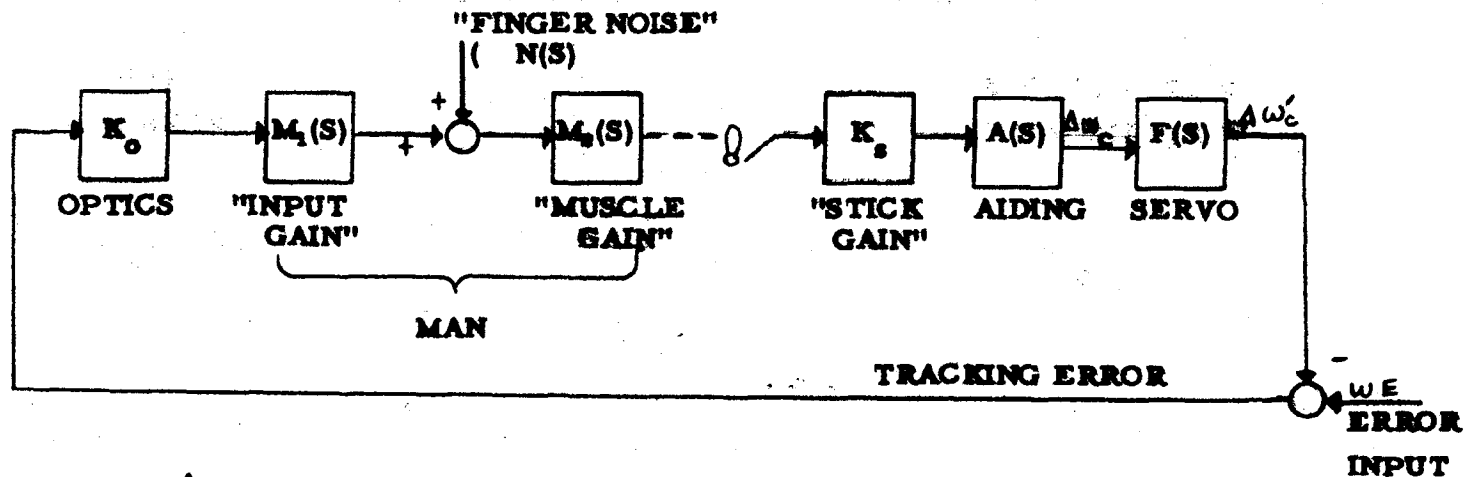


0.5

SECONDS

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$$G(s) \triangleq K_o M_1(s) K_s A(s) F(s)$$

- IN PASS BAND ( $G(s) > 1$ )

$$\Delta \omega^2 = \int_0^{BW} \left( \frac{\omega_E(s)}{G(s)} \right)^2 + \left( \frac{N(s)}{K_o M_1(s)} \right)^2 df$$

BW = BANDWIDTH  
 f = FREQUENCY

- ASSUME MAN'S "MUSCLE GAIN" IS ADAPTIVE TO INPUT ERROR OVER RANGE OF INTEREST

/ THEN HE INCREASES  $G(s)$  SUCH THAT  $\frac{\omega_E s}{G(s)} = \text{CONSTANT}$   
 WITH BW PROP TO MUSCLE GAIN

/  $\Delta \omega$  IS THEN PROPORTIONAL TO (BANDWIDTH)<sup>1/2</sup>

- WITH ACCELERATION, AIDING, ONE ALLOWS A REDUCTION IN "MUSCLE GAIN" BY RAISING  $G(s)$  IN THE LOW FREQUENCY REGION, THUS IMPROVING STEADY STATE RESPONSE.

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FUTURE EFFORT

● **SIMULATOR IMPROVEMENT**

- **REDUCE EFFECT OR TABLE STICTION - (MECH. MODS OR SCALING)**
- **REDUCE AVAILABLE ACQUISITION TIME**
- **IMPROVE CONTROL STICK FEEL - (DAMPING & SPRING RETURN)**
- **RESCALE COMPUTER SIMULATION FOR HIGHER RATE AIDING ERRORS**
- **PROVIDE FOR TESTING VARIOUS STICK FUNCTIONS**

● **ANALYTICAL EFFORT**

- **DEFINE A "USEFUL" MODEL FOR MAN IN THIS FUNCTION**
- **DETERMINE DESIGN/STABILITY CRITERIA FOR ACCEL/JERK  
STICK FUNCTION AUGMENTATION**
- **GENERATE RATE ERROR INPUT DATA FOR THE VARIOUS ERROR SOURCE  
CONSISTENT WITH THE ANALOG BACKUP DESIGN: CORRELATE  
POINTING AND RATE ERRORS**
- **DETERMINE SIMPLE MINIMAL TRANSIENT ACQUISITION TO PRIMARY  
HANDOVER TECHNIQUES**

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FUTURE EFFORT(CONT)

● SIMULATION

● STICK FUNCTION OPTIMIZATION FOR TRACKING

- STICK FEEL
- AUGMENTATION: ACCEL + HIGHER ORDER AIDING
- RATE ERROR LEVEL FROM 1% TO 10% V/h
- VERIFICATION OF MODEL/STABILITY BOUNDARIES FOR MAN.

● INITIALIZATION STUDY - MINIMIZE ACQUISITION AND RATE KILLING TIME

- OPERATOR TRAINING
- ACQUISITION TO PRIMARY HANDOFF TECHNIQUES
- ACQUISITION STICK FUNCTION
- PRIMARY STICK FUNCTION

● ESTABLISH TRADEOFFS BETWEEN SETTLING TIME AND TRACKING

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SUMMARY

- 0 - SIMULATION EQUIPMENT INADEQUATE TO SHOW FULL PERFORMANCE CAPABILITY
- 1 - MAN CAN PRODUCE SATISFACTORY RESULTS WITH INPUT RATE ERRORS AS HIGH AS 10% V/h
- 2 - MAN APPEARS TO BE GAIN ADAPTIVE  
STICK GAIN ADJUSTED FOR INDIVIDUAL COMFORT
- 3 - STICK AUGMENTATION BY HIGHER ORDER FUNCTIONS IS A FRUITFUL APPROACH TO IMPROVE PERFORMANCE
- 4 - SETTLING TIME IS REDUCED BY EXPERIENCE

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ANALOG ACQUISITION & TRACKING BACKUP

- **CONCEPT**
  - PROVIDE EFFECTIVE BACKUP FOR COMPUTER & COMMAND S/S FAILURE
  - MINIMAL INTERFACE WITH PRIMARY HARDWARE
  - SIMPLE AS POSSIBLE TO ALLOW MISSION CONTINUATION
  
- **POINTING ACCURACY**
  - UNAIDED: 1 - 2 DEG. ; AIDED: 0.1 - 0.2 DEGREE
  
- **RATE ACCURACY**
  - UNAIDED: 3 - 5% V/h ; AIDED: 0.1 - 0.2% V/h
  
- **EXCLUSIONS/SIMPLIFICATIONS**
  - NO NAVIGATIONAL UPDATING
  - NO AUTOMATIC MODE
  - SINGLE TARGETS ONLY. (NO CLUSTER CAPABILITY)
  - INDEPENDENT OF ACTS ELECTRONICS
  - MANUAL OR MINIMAL COMMAND UNIT INPUTS ONLY

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**FAILURE MODE COMPARISON**

<b><u>FAILED ELEMENTS</u></b>	<b><u>ANALOG BACKUP</u></b>	<b><u>NO ANALOG BACKUP</u></b>	<b><u>UNMANNED</u></b>
<b>DATA READOUT</b>	<b>OK</b>	<b>OK</b>	<b>OK</b>
<b>ONE ACQ SCOPE</b>	<b>OK</b>	<b>OK</b>	<b>NA</b>
<b>ONE CONSOLE</b>	<b>OK</b>	<b>OK</b>	<b>NA</b>
<b>DRAGLAR ACCEL</b>	<b>OK</b>	<b>OK</b>	<b>MARGINAL/DEAD</b>
<b>ATTITUDE CONTROL</b>	<b>OK, EXCEPT FOR VALVES</b>	<b>OK, EXCEPT FOR VALVES</b>	<b>DEAD</b>
<b>V/H SENSOR</b>	<b>OK</b>	<b>OK</b>	<b>MARGINAL/DEAD</b>
<b>STAR TRACKER</b>	<b>OK</b>	<b>OK</b>	<b>MARGINAL</b>
<b>FORMAT SERVO</b>	<b>OK</b>	<b>OK</b>	<b>MARGINAL</b>
<b>DIGITAL COMPUTER (S)</b>	<b>OK</b>	<b>DEAD</b>	<b>DEAD</b>
<b>COMMAND SUBSYSTEM</b>	<b>OK (LESS TARGETS)</b>	<b>DEAD</b>	<b>DEAD</b>
<b>FOCUS SERVO</b>	<b>MARGINAL</b>	<b>MARGINAL</b>	<b>MARGINAL</b>
<b>PRIMARY SERVO</b>	<b>BACKS UP ONLY SHAFT ENCODERS</b>	<b>DEAD</b>	<b>DEAD</b>

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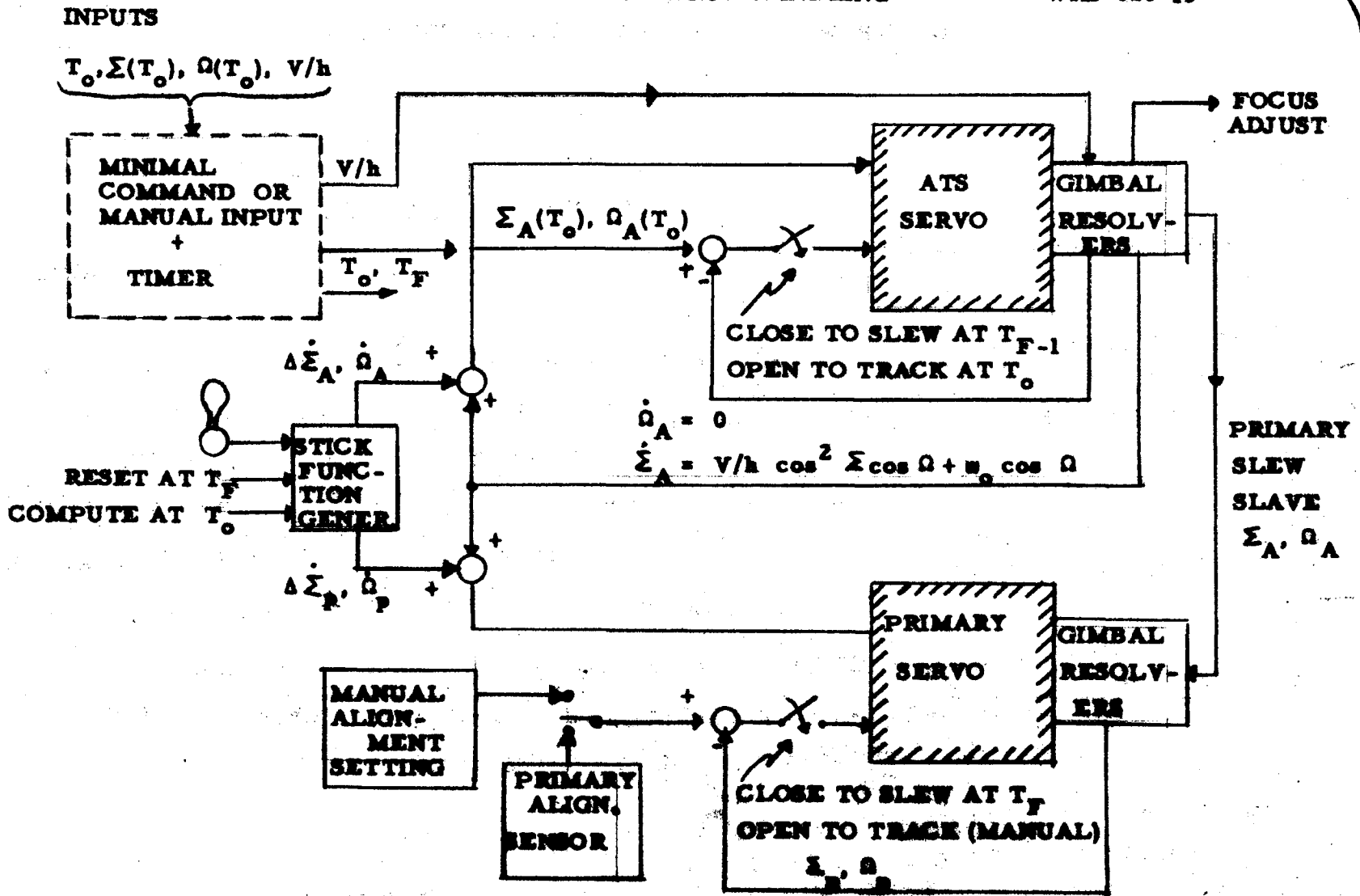
BACKUP DRIVE APPROACH

- SERVO CONTROL
  - RESOLVER CHAIN TRACKING FUNCTION GENERATION/CONTROL
  - RESOLVERS GEARED TO SERVO GIMBALS
  - ATS SERVO USED AS A COMPUTER
  - ESTIMATED WEIGHT: < 20 LBS
  - ESTIMATED POWER: < 25 WATTS
- COMMAND FUNCTION
  - MINIMAL COMMAND UNIT OR MANUAL RESOLVER SETTINGS & TIMER
  - INPUTS: STEREO AT ACQUISITION, OBLIQUITY,  $V/h$ , ACQUISITION TIME;  
STEREO AT ACQUISITION FIXED FOR A PASS

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BACKUP DRIVE BLOCK DIAGRAM

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$$\omega_y = \left\{ \frac{\frac{1}{2}}{b_x + \tan \theta (s \Omega b_y - c \Omega b_z)} \right\} \left\{ c^2 \Omega \frac{V}{h} + c \Omega \omega^0 \right. \\ \left. - \tan \theta (\omega_y^b b_z - \omega_z^b b_y) + s \Omega (\omega_z^b - \omega_x^b b_z) - c \Omega (\omega_x^b b_y - \dot{\theta}) \right. \\ \left. + [(\tan \theta s \Omega - c \Omega c^2 \Omega) b_z^2 + (s \Omega + \tan \theta c \Omega)(s \Omega b_y - c \Omega b_z) + c \Omega s \Omega b_y b_z] \dot{\lambda}_x \right. \\ \left. + [s \Omega s \Omega + (s^2 \Omega (\tan \theta s \Omega - c \Omega) - \tan \theta c \Omega) b_y + s \Omega c \Omega (c \Omega - \tan \theta (1 + s \Omega) b_z)] \dot{\lambda}_y \right. \\ \left. + [-s \Omega c \Omega + s \Omega c \Omega (c \Omega - \tan \theta (1 + s \Omega)) b_y + (c^2 \Omega (\tan \theta s \Omega - c \Omega) - \tan \theta s^2 \Omega) b_z] \dot{\lambda}_z \right\}$$

$$\omega_x = \left\{ \frac{1}{b_x + \tan \theta (s \Omega b_y - c \Omega b_z)} \right\} \left\{ (s \Omega b_y - c \Omega b_z - \tan \theta) (s \Omega \omega_y^b - c \Omega \omega_z^b) + \frac{1}{c \Omega} (s \Omega b_y - c \Omega b_z) \omega_x^b \right. \\ \left. - [s \Omega c \Omega (b_y^2 - b_z^2) - \tan \theta (c \Omega b_y + s \Omega b_z - c \Omega b_y b_z)] \dot{\lambda}_x \right. \\ \left. - \left[ \frac{c \Omega}{c \Omega} + s \Omega (c \Omega b_y + s \Omega b_z) \right] \dot{\lambda}_y - \left[ \frac{s \Omega}{c \Omega} - c \Omega (c \Omega b_y + s \Omega b_z) \right] \dot{\lambda}_z \right\}$$

$\omega_x, \omega_y$  = inertial pitch & roll gimbal rates

$\Omega$  = roll gimbal angle

$\Sigma = 2\theta - \pi/2$  = mirror stereo angle

$\underline{b}$  = optical axis vector

$\omega_b$  = vehicle inertial rate

$\dot{\lambda}$  = line of sight rate

### BASELINE RATE EQUATIONS

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SMEAR ANALYSIS - ACQUISITION SCOPE

+ 30°  $\epsilon$ , 0°  $\Omega$ , 80 n. mi.

<u>ERROR SOURCE</u>	<u>IN-TRACK SMEAR</u>	<u>°/SEC</u>	<u>X-TRACK SMEAR</u>
VEHICLE ATTITUDE (.5° ALL AXES)	.011	<del>0.023</del>	.023
VEHICLE RATES (.02°/SEC ALL AXES)	.02		.022
EPHEMERIS (4 K, 2 K, 2 K FT)	.01		-
ORBITAL RATE (.2%, .1° EQUIV. 500 FT/SEC)	.007		.005
SCOPE BASE ALIGNMENT (.5°)	.011		.023
ACQUISITION SCOPE ANGLES			
$\Sigma$ (1° SET, 1° STANDOFF)	.044		-
$\Omega$ (1° SET)	-		-
ACQUISITION SCOPE RATES (.015°/SEC)	.03		.013
SERVO COMPUTER ACCURACY (1%)	.03		.03
	RSS	.081°/SEC	.051°/SEC
POINT ACQUISITION TO TARGET (.15°)	.005	(REMOVE .044 ABOVE)	-
	RSS	.067°/SEC	.051°/SEC
1% V/h $\approx$ .03°/SEC.			

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SMEAR ANALYSIS - PRIMARY W/O MANUAL CONTROL

$30^\circ \Sigma$ ,  $0^\circ \Omega$ , 80 n. mi.

<u>ERROR SOURCE</u>	<u>IN-TRACK SMEAR</u>	<u>X-TRACK SMEAR</u>
ACQ SCOPE HANDOVER	.067 °/SEC	.051
SUBTRACT ROLL RATE CONTRIBUTOR (USING INERTIAL DRIVE)	--	(.017)
OPTICAL AXIS ALIGNMENT ( $1^\circ$ )	.038	.02
POINTING ERROR ( $.15^\circ$ )	.005	
RATE ERROR OF SERVO ( $.005^\circ$ /SEC)	.01	.004
	<hr/>	<hr/>
RSS ERROR AT $\Sigma = +30^\circ$	.079 °/SEC	.052 °/SEC
COMPUTER ERROR INCREMENT TO $\Sigma = -30^\circ$	.12	---
	<hr/>	<hr/>
RSS ERROR AT $\Sigma = -30^\circ$	.143 °/SEC	.052 °/SEC

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FUTURE EFFORT

- **ANALYTICAL**
  - **DETAIL DESIGN OF CONCEPT**
  - **DECIDE ON COMMAND FUNCTION APPROACH (PERHAPS USE BOTH)**
  - **DETERMINE METHOD OF MECHANICAL INTEGRATION:  
INTEGRATE INTO BASELINE**
  - **FIX STICK FUNCTION**
  - **DETERMINE FEASIBLE OPERATIONAL CYCLE TIMES**
  
- **MANAGERIAL**
  - **EVALUATE COST EFFECTIVENESS OF APPROACH (ES)**
  - **REPLACE ONE COMPUTER WITH BACKUP OR ADD TO PRESENT  
SYSTEM?**
  - **EVALUATE IMPACT ON SCHEDULE, TEST, ETC.**
  - **COST ( < 100 K/COPY ESTIMATED)**
  - **KEEP IT SIMPLE - IT'S A BACKUP!**

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